

Dynamic Surface Control Approach for UAV Firefighting System

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Outline

1. Motivation

2. Dynamic Surface Control

3. Controller Design

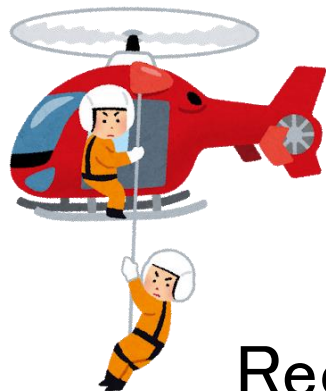
4. Numerical Simulation

5. Conclusion

Background

Aircraft capability to cope with disasters

Rescue



Transportation



Reconnaissance



Background

Aerial Firefighting

Advantage

- High workload for the pilot
- No need for a fire hydrant

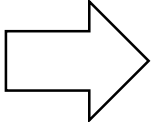
- Leading to risk for mission
- The ability to drop a large amount of water

➔ Autonomous control addresses this problem
 Great performance in the case of forest fire



Aerial Firefighting (USAF)

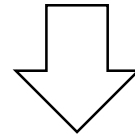
Problems for designing UAV firefighting system

Dramatical mass variation  **Time varying system**

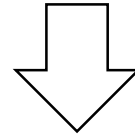
- Effect by unmeasurable force with mass variation
- Strong nonlinearity is appeared at the dynamics

Problems for designing UAV firefighting system

Conventional method
(State feedback control)

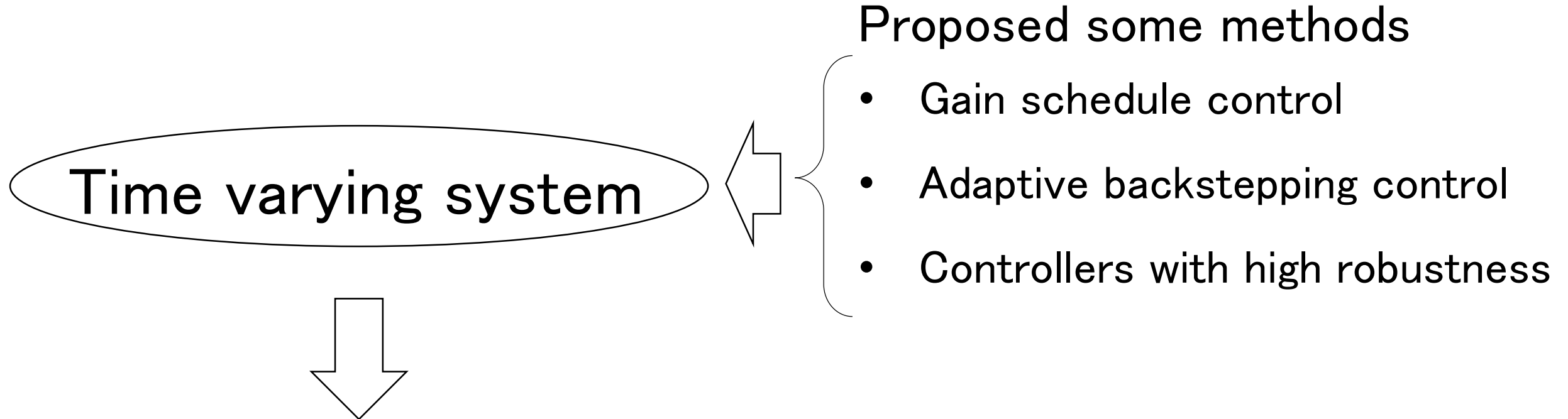


Time varying system



Deterioration control performance and Flight instability

Problems for designing UAV firefighting system



These methods have left some problems for application.

Proposed method

Dynamic Surface Control

⇒ DSC method incorporates a filter between each subsystem to simplify the back-stepping control.
with Extended State Observer

Extended State Observer is adopted into the UAV firefighting system.

⇒ To compensate the effect by unmeasurable quantities

- Aerodynamic force and moment
- Disturbance
- The effect by time varying system

Objectives

- Designing flight control system for the UAV firefighting system.
- Verifying the effectiveness of proposed method by the numerical simulation.

Works to do

- Applying DSC with ESO into the UAV firefighting system.
- Comparison of control performance (DSC with ESO vs LQI)

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In the nonlinear controllers

Back-stepping control \Rightarrow effective method

Virtual Input

However

$$x_{(i+1)d} = \frac{1}{g_i} (-k_i s_i + \dot{x}_{id} - f_i - g_{i-1} s_{i-1}) \quad \because s_i = x_i - x_{id}$$

This method faces difficulty for application.

x_{id} includes uncertainty

\Rightarrow Explosion terms arise in virtual input.

Tedious and complex for application

Dynamic surface control

Virtual Input

$$x_{ic} = \frac{1}{g_{i-1}} (-k_{i-1} s_{i-1} + \dot{x}_{i-1d} - f_{i-1}) \quad (\text{i-1 th})$$

$$\because s_i = x_i - x_{id}$$

2nd Order Filter \rightarrow Smoothing derivative of x_{id}

\dot{x}_{id}

$$\ddot{x}_{id} + 2\zeta\omega\dot{x}_{id} + \omega^2 x_{id} = \omega^2 x_{ic}$$

\rightarrow Relief sudden signal rise

Actual Input

$$x_{(i+1)c} = \frac{1}{g_i} (-k_i s_i + \dot{x}_{id} - f_i) \quad (\text{i th}) \quad (i = 1, \dots, n-1)$$

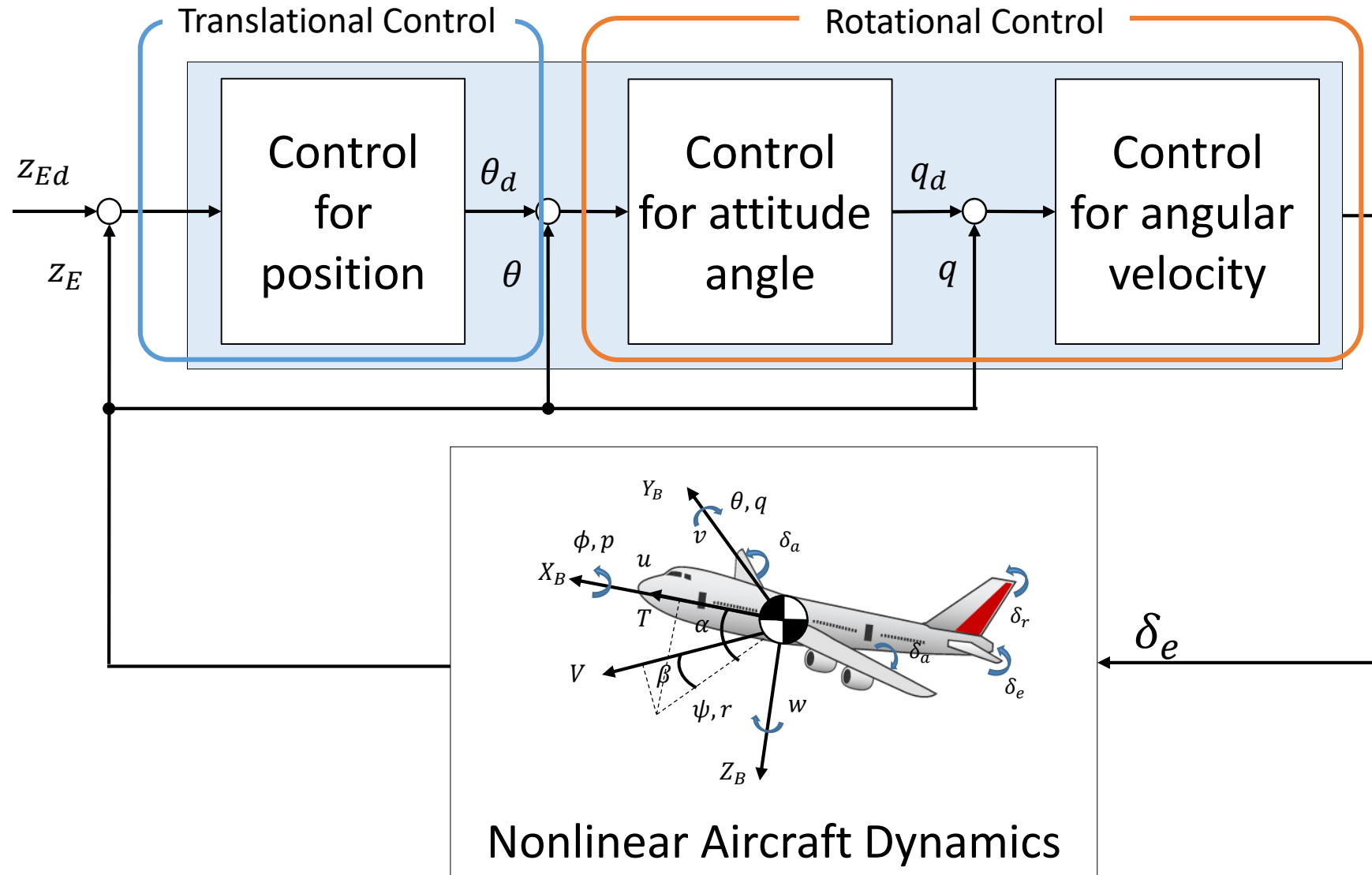
$$u = \frac{1}{g_n} (-k_n s_n + \dot{x}_{nd} - f_n)$$

\rightarrow The calculation of virtual input x_{ic} is simplified

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Flight Control System



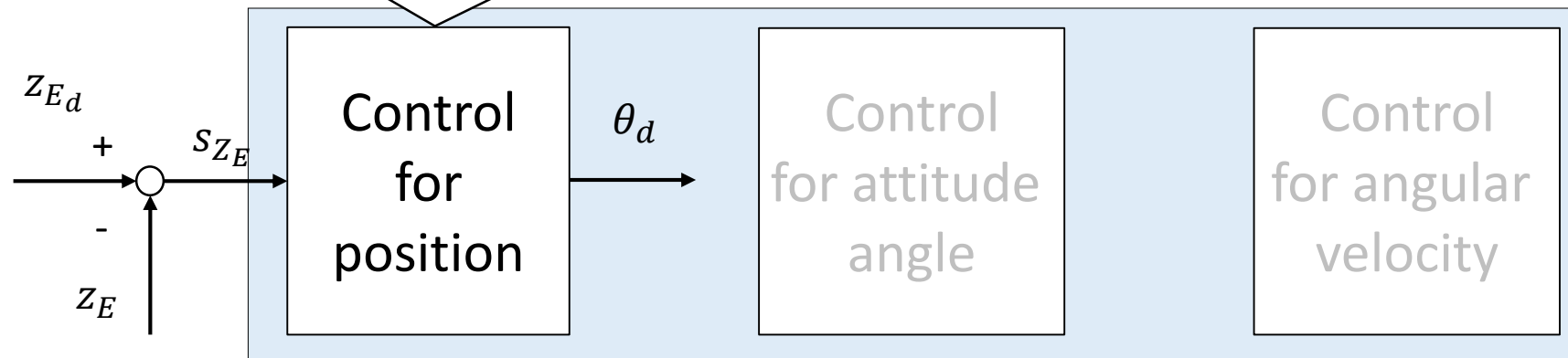
Translational control

Control for position

Tracking error

$$s_{z_E} = z_E - z_{Ed}$$

$$\theta_d = \arcsin \frac{(-k_{zP}s_{z_E} - k_{zI} \int s_{z_E} dt - k_{zD}\dot{s}_{z_E})}{V}$$



Dynamic Transformation

Aircraft dynamics

$$\dot{\theta} = q \quad \dot{q} = \frac{1}{I_{yy}} \left(\frac{\rho V^2 S \bar{c}}{2} C_m + z_p T \right) + d$$

Transformation

Nonlinear system

$$\dot{x}_1 = f_1 + g_1 x_2 \quad \dot{x}_2 = (f_{2n} + \Delta f_2) + (g_{2n} + \Delta g_2) \delta_e + d$$

$$x_1 = \theta$$

$$f_1 = 0, g_1 = 1$$

$$x_2 = q$$

$$f_2 = \frac{\rho V^2 S \bar{c}}{2 I_{yy}} \left\{ \frac{\rho V^2 S \bar{c}}{2 I_{yy_0}} \left(\frac{C_m}{2 V} \left(C_{m\alpha} \dot{\alpha} + C_{mq} q \right) + \frac{z_p T}{I_{yy_0}} \right) + \frac{z_p T}{I_{yy}} \right\}$$

$$g g_2 = \frac{\rho V^2 S \bar{c}}{2 I_{yy_0}} C_{m\delta_e}$$

Rotational control

Control for attitude angle

Tracking error

$$s_1 = \theta - \theta_d$$

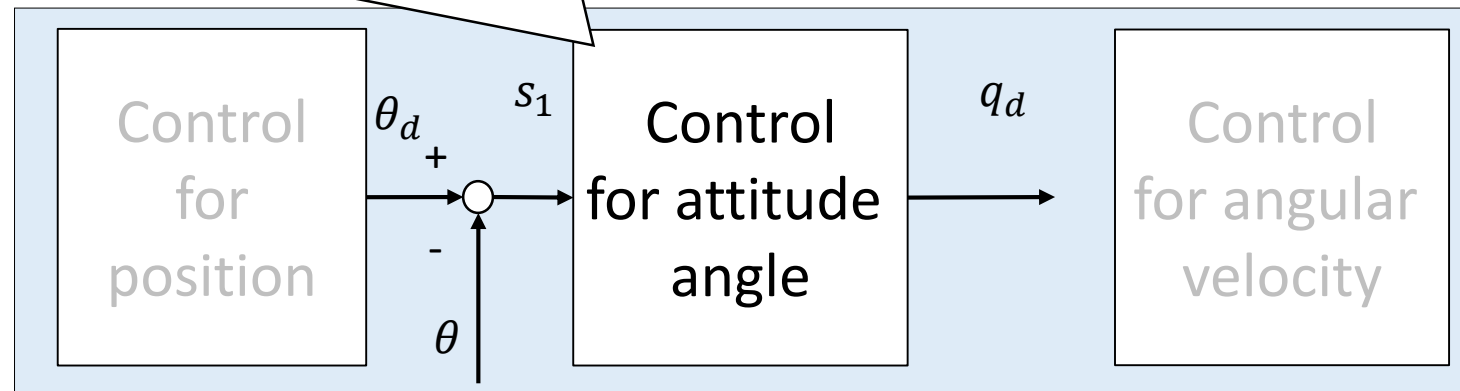
Virtual Input

$$x_{2c} = \frac{(-k_1 s_1 + \dot{\theta}_d)}{g_1}$$

2nd order filter

$$\ddot{x}_{2d} + 2\zeta\omega\dot{x}_{2d} + \omega^2 x_{2d} = \omega^2 x_{2c}$$

$$\therefore x_{2d} \rightarrow q_d$$



Rotational control

Control for angular velocity

Tracking error

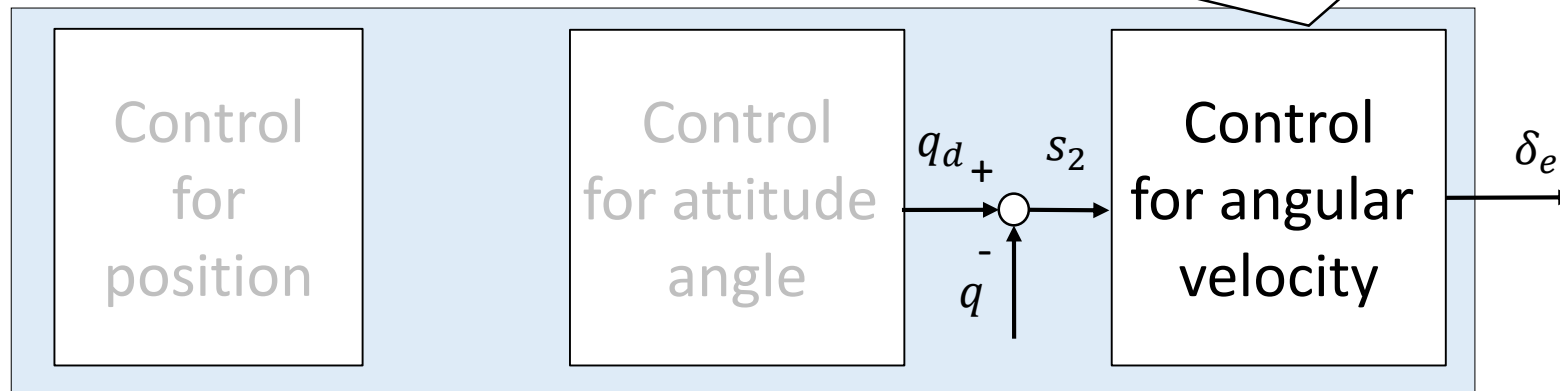
$$s_2 = \dot{q} - \dot{q}_d$$

Actual Input

$$\delta_e = \frac{(-f_{2n} - k_2 s_2 + \dot{q} - \hat{D}_2)}{g_{2n}}$$

$$\begin{aligned} e_2 &= \hat{q} - q \\ \dot{\hat{q}} &= \hat{D}_2 - k_{o1} e_2 + f_{2n} + g_{2N} \delta_e \end{aligned}$$

$$\dot{\hat{D}}_2 = k_{o2} e_2$$



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Setting



Specification

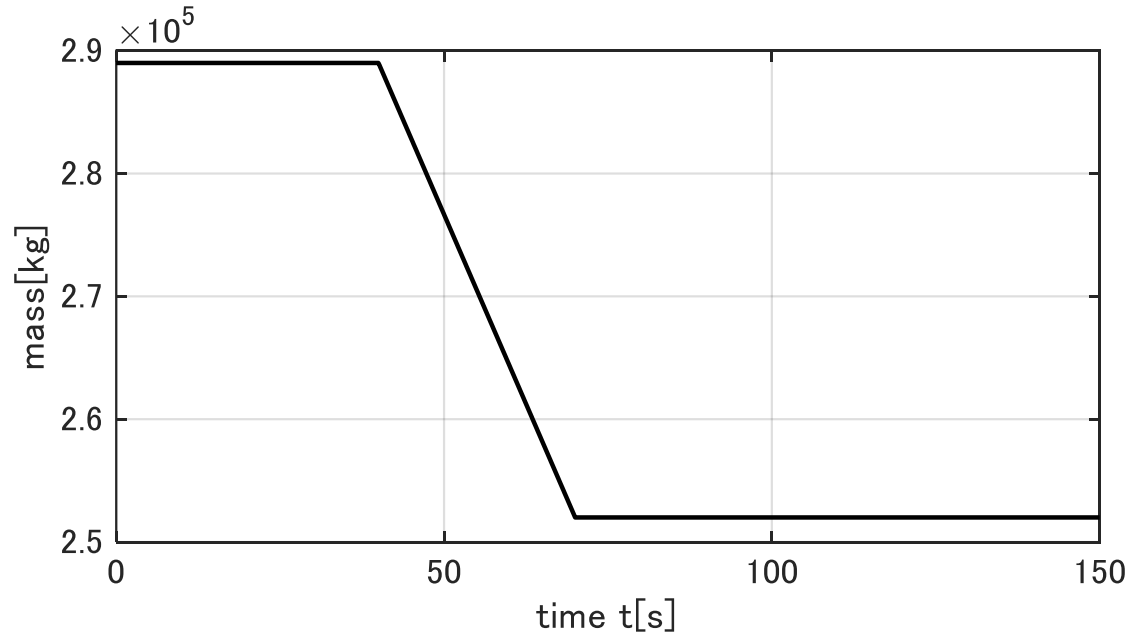
Aircraft	B747
Wing area S [m ²]	511
Wing span b [m]	59.6
MAC \bar{c} [m]	8.32
Mass m [kg]	289,000

Initial values

Velocity V_0 [m/s]	84.88
Pitch angle θ_0 [rad]	0.02564
Pitch angular velocity q [rad/s]	0
Angle of attack α_0 [rad]	0.02564
Thrust trim T_{trim} [N]	268,425

Setting

Mass variation



Disturbance

$$\dot{q} = \frac{1}{I_{yy}} \left(\frac{\rho V^2 S \bar{c}}{2} C_m + z_p T \right) + d$$

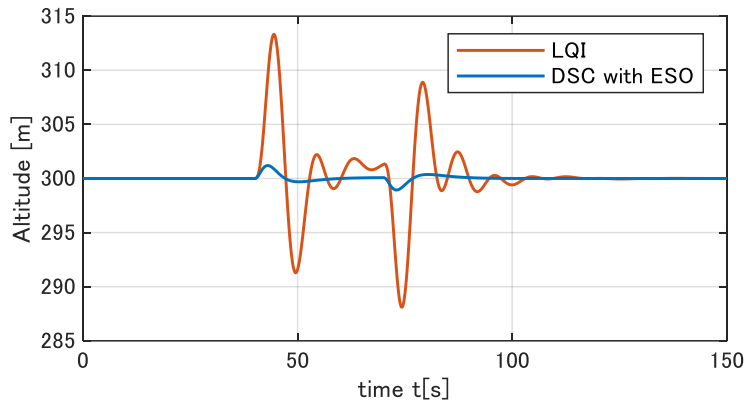
$$d = \begin{cases} 0.1 & 40 \leq t \leq 70 \\ 0 & \text{others} \end{cases}$$

Comparison control performance between

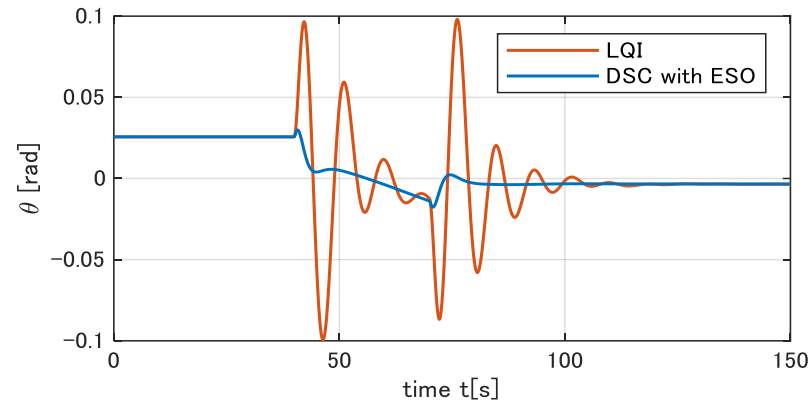
DSC with ESO and LQI control

Results (LQI vs DSC with ESO)

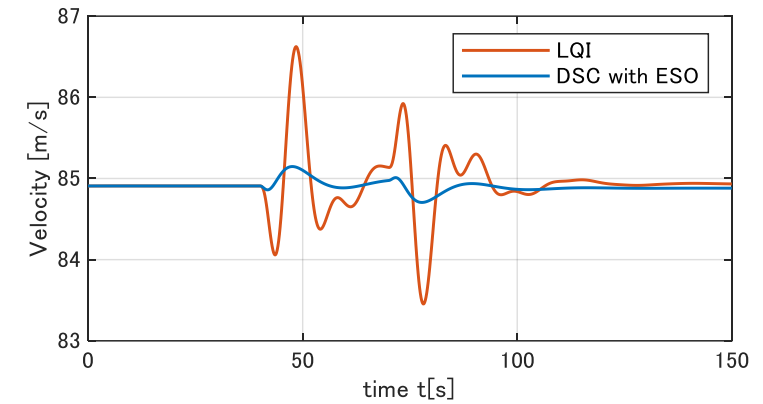
Altitude



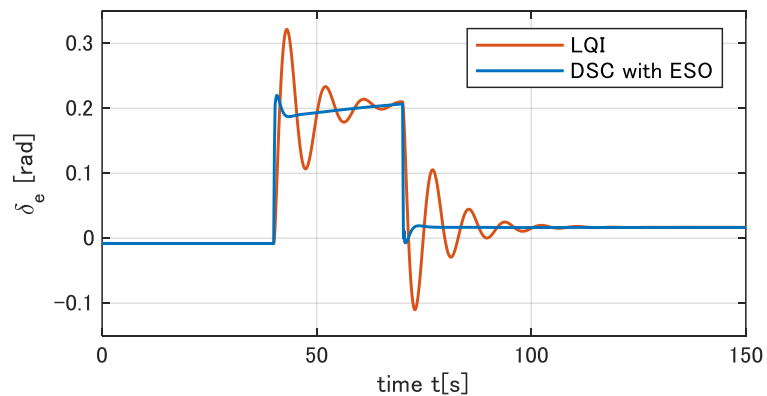
Pitch angle



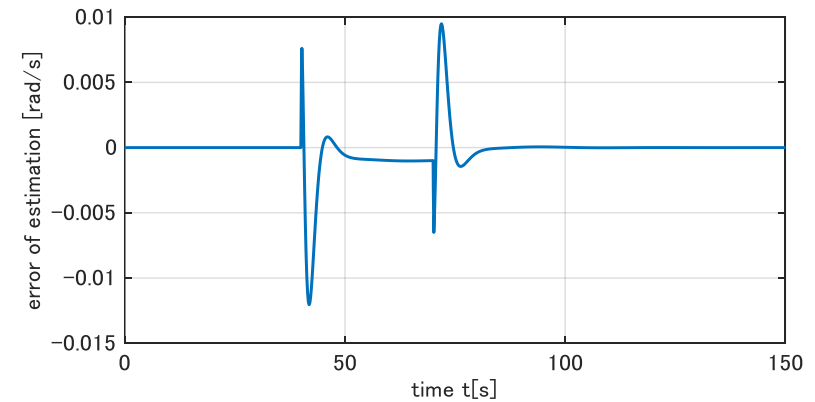
Velocity



Elevator deflection

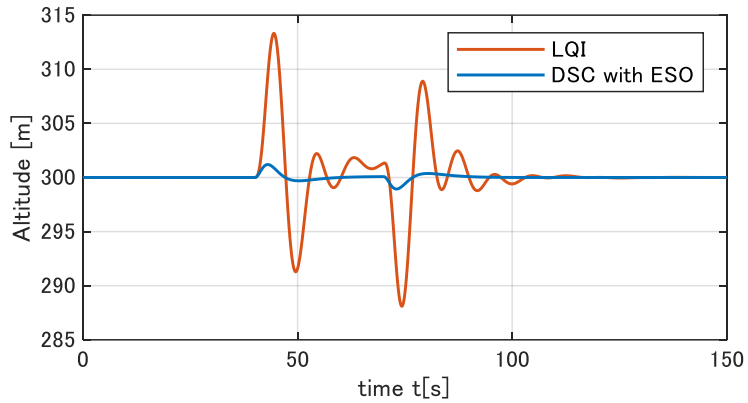


Error of estimation

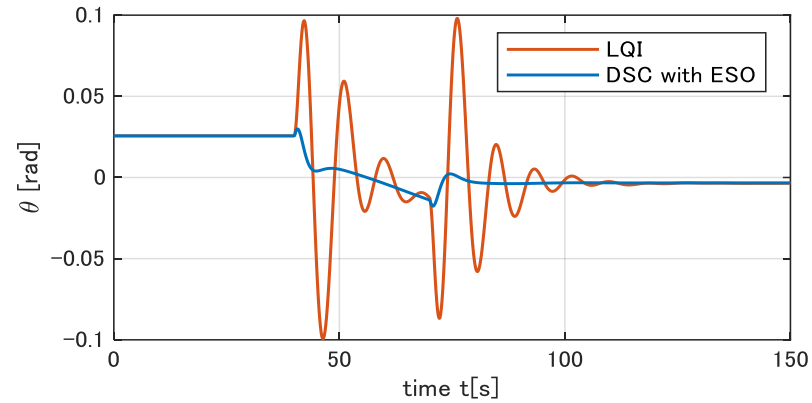


Results (LQI vs DSC with ESO)

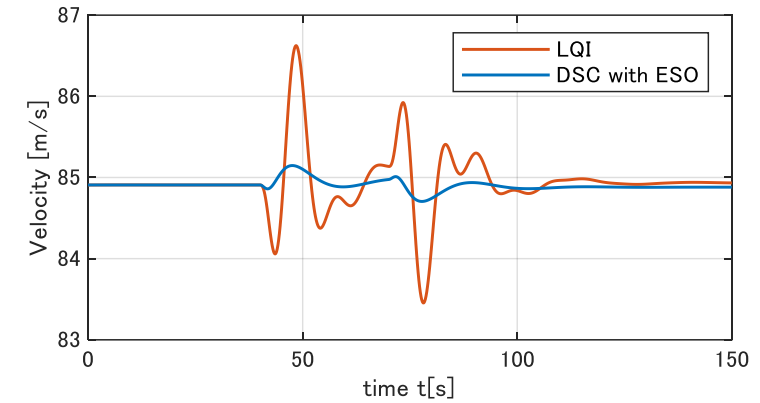
Altitude



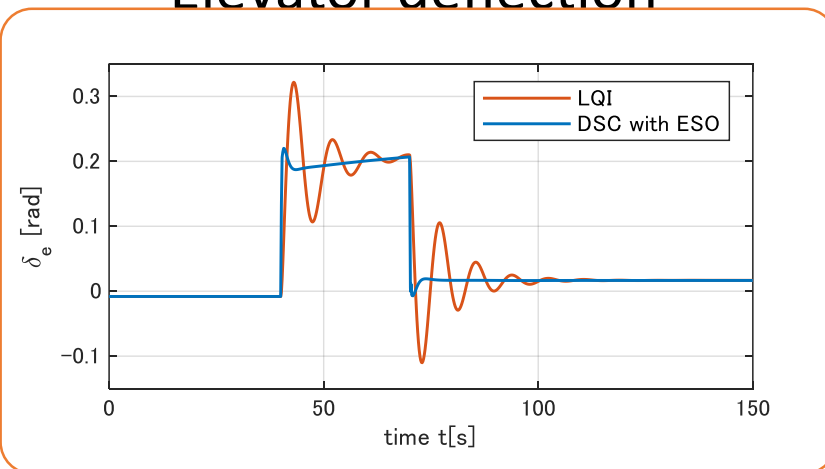
Pitch angle



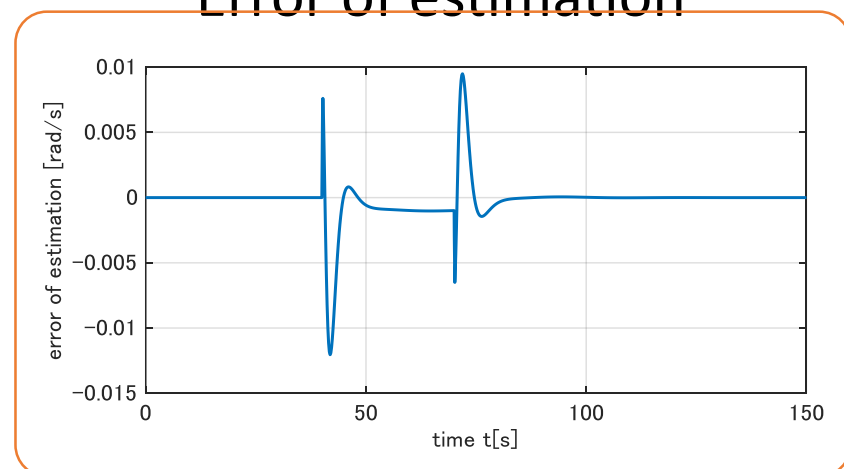
Velocity



Elevator deflection



Error of estimation



5.Conclusion

- We propose the flight control system for UAV fire fighting system by using DSC with ESO.
- The numerical simulation results show the effectiveness of the proposed method.

Thank you for your attention.